



CHMT 2019 – Enschede

Rotor Cooling Concept for the ASuMED Superconductive Motor

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CHMT 2019 – Cryogenic Heat and Mass Transfer, Enschede
Demaco, It's all about Cryogenius!

Outline

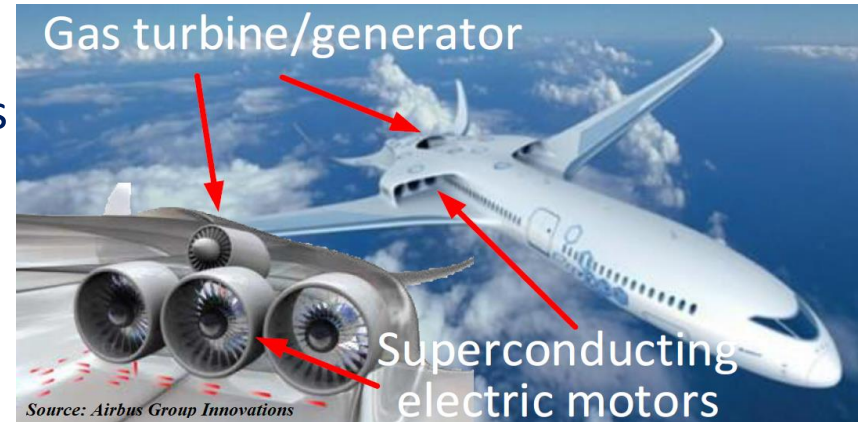


- Introduction
- Motor Cryostat Concept
- Rotor Cooling System
- Heat transfer & flow analysis
- Status and outlook



ASuMED: Advanced Superconducting Motor Experimental Demonstrator

- Air traffic grows 5% each year
- Flightpath 2050 fuel burn and emissions reduction (compared to 2000):
 - 75% CO₂ reduction
 - 90% NO_x and PM reduction
 - 65% noise reduction



Funded by Horizon 2020 programme:



Funded by the
European Commission
Grant No 723119

*“ASuMED has received funding from the European Union’s Horizon 2020 research and innovation programme under grant agreement No 723119”
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ASuMED: Advanced Superconducting Motor Experimental Demonstrator

- **First fully superconductive motor** prototype for aerospace applications
- **1 MW** power at 6000 rpm
- Overall **efficiency** higher than **99%**



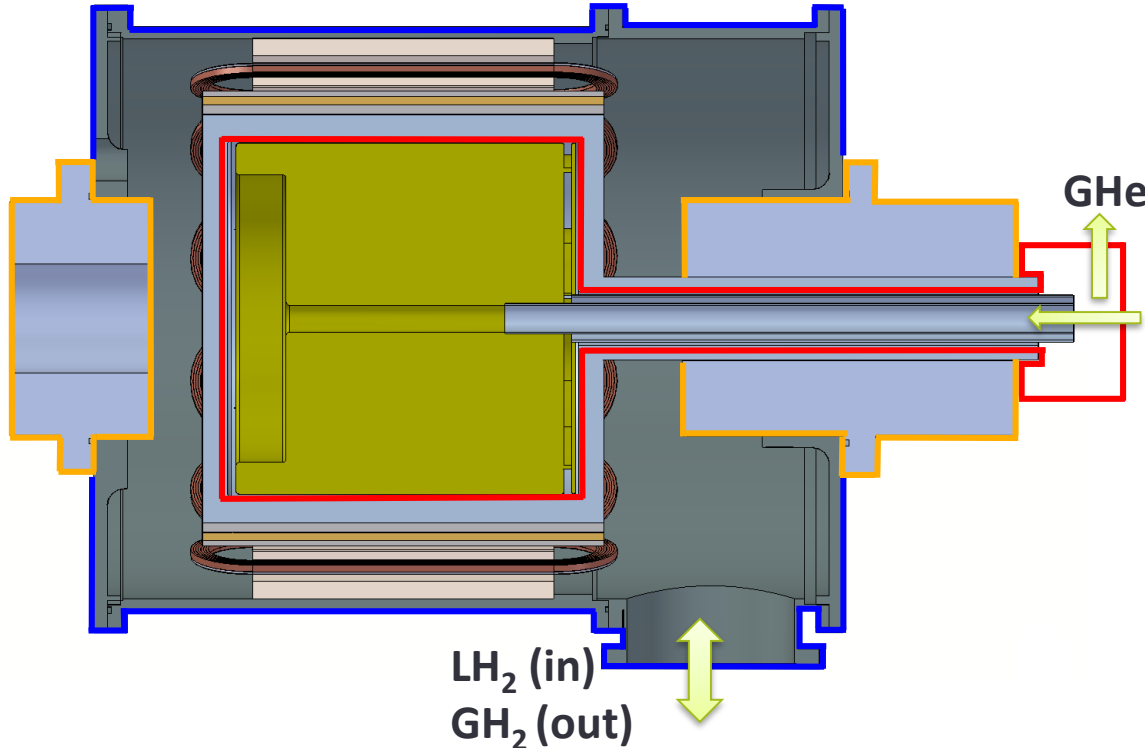
- **Rotor cooling system: design, building, testing**
- **Cryogenic advice**
- **Conditioning equipment for test: design, building, testing**



Motor Cryostat Concept



Dual-Cryostat Concept: two separated cryostats for rotor and stator



Stator

- Cryogen: Liquid Hydrogen
- Designed by Oswald

Rotor

- Cryogen: Gaseous Helium
- Designed by Demaco & UCAM

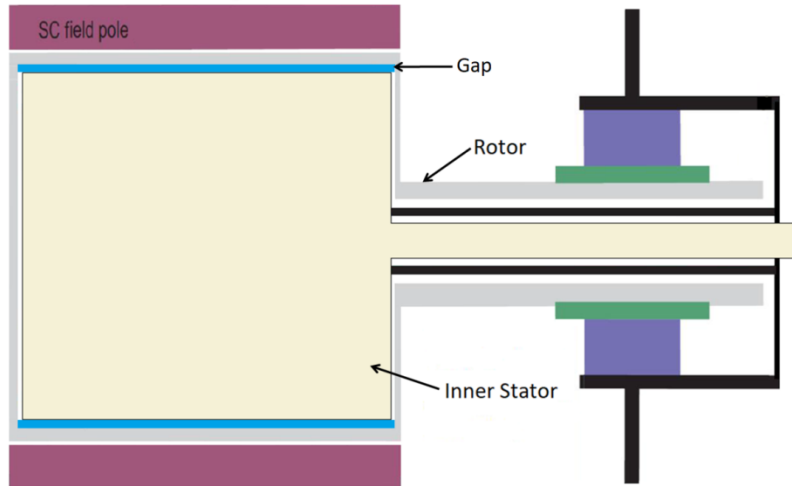
Rotary Seal

- Ferrofluidic seal
- Being tested

Rotor Cooling System



Rotor Cryostat Reference Model



Rotor – SC Stacks – Rotating

- HT Superconducting stacks
- Stacks temperature 30K – 35K

Inner Stator – Stationary

- Cooling fluid
 - Helium
 - Inlet Temperature 25K
 - Operating pressure 2 bar (a)

Gap

- 2 mm high

Required Rotor cooling power: 150 W

- Heat generated in the SC Rotor stacks + heat leak into the system

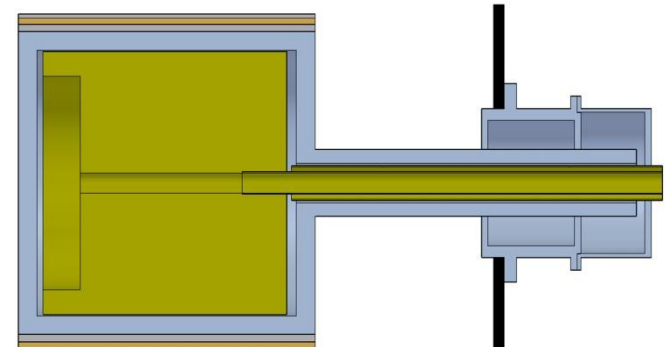


Rotor Cooling Concepts

- Conduction based cooling system: not feasible
- **Convection based system: potential to achieve required cooling power**

Externally Controlled Rotor Cooling System: CONVECTION based system

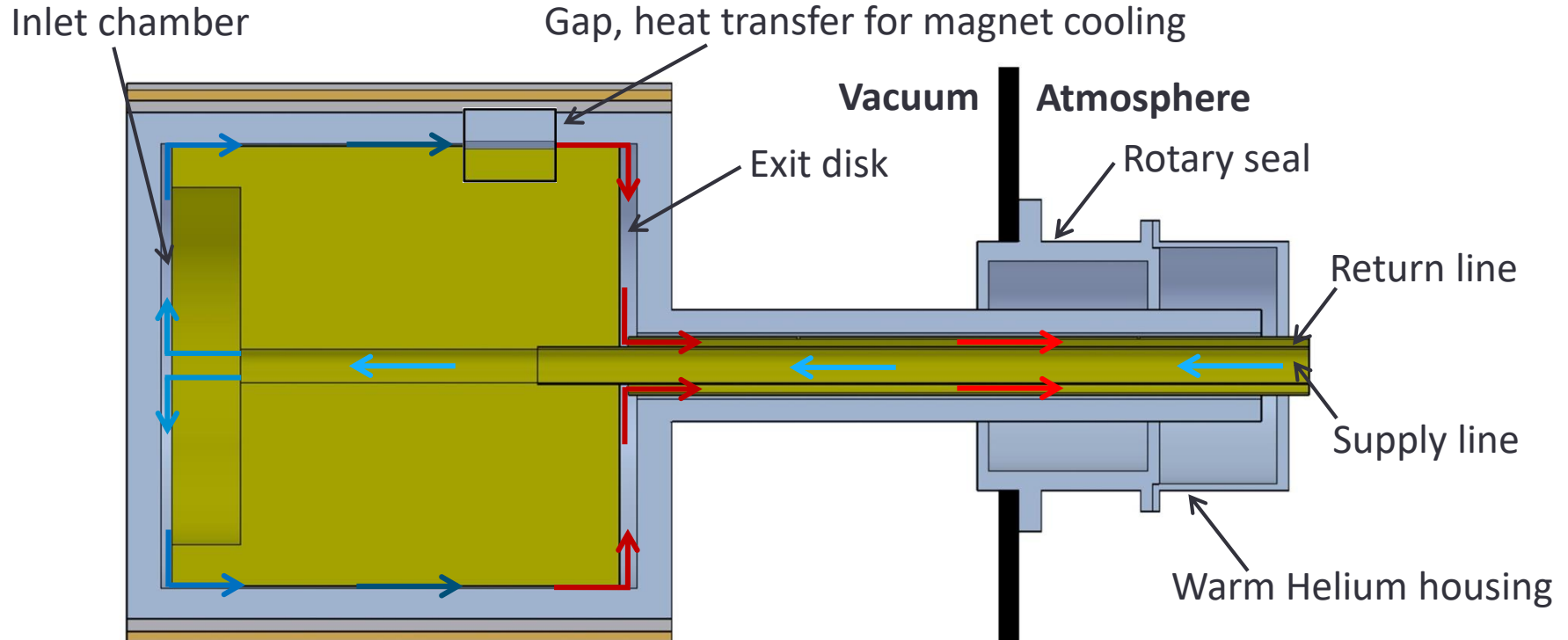
- Forced Circulation of cooling gas through the system
- Challenging system characterisation:
 - Rotating outer cylinder, ROTOR
 - Stationary inner cylinder, INNER STATOR
 - **Influence of outer cylinder rotation unknown**



Rotor Cryostat Design



Externally Controlled Rotor Cooling System, forced convection





Engineering approach to analyse and size the Rotor Cooling System

- Goal: minimize design risk in an uncertain situation with limited resources

Analysis methods

- General assessment of flow types, literature study
 - Similarities with **Taylor-Couette flow**
- Classical analysis based on Reynolds and Nusselt numbers
 - Flat plate, pipe, **stationary annulus**
- FEM analysis (COMSOL)

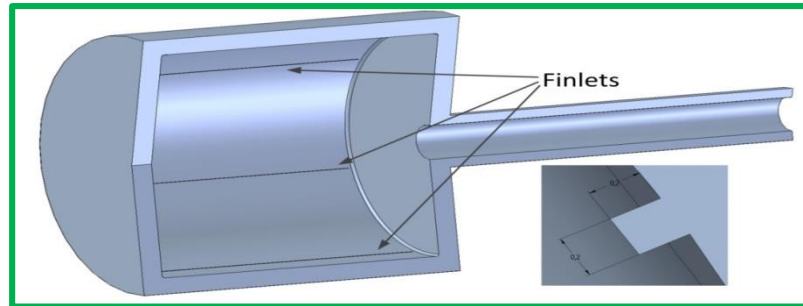
Design

- Basic sizing based on worst case results from different kinds of analysis
- Additional measures prepared to improve performance if required



Similarities with Taylor-Couette flow

- Taylor-Couette flow:
 - “Flow between independently rotating coaxial cylinders in a closed system”
 - Speciality of University of Twente – Physics of Fluids group
 - Wall roughness important parameter
 - Finlets give remarkable increase of heat transfer (6 in proposed design)



- Standard FEM codes of limited value



Classical analysis of forced convection based system

- Turbulent flow: $Re = 14000$
- System characterisation:
 - Rotating outer cylinder, ROTOR
 - Stationary inner cylinder, INNER STATOR
- Literature study to define Nusselt number
 - Cylinders with walls at rest
 - **Influence of outer cylinder rotation unknown**

Geometry	Nu
Flat Plate	70
Pipe	45
Stationary Annulus	35



Nusselt Number = 20

Preliminary heat transfer analysis, forced circulation

Scenario	ΔT (K)	Q_{gap} (W)	Q_{goal} ratio
1	2	41	28 %
2	5	107	71 %
3	10	226	150 %



**POTENTIAL TO ACHIEVE
REQUIRED COOLING
POWER**



Details for analysis – FEM analysis

- Helium **mass flow** through the system: **20 g/s**
 - From $Re = 14000$
- **Pressure** in the system: 2 bar(a)

Analysed Cases and Operating modes

Analysis Case	ΔT (K)	Ω (rpm)	
AC 1.1	2	0	Magnetisation mode
AC 1.2	2	1200	
AC 1.3	2	3000	
AC 1.4	2	6000	Normal Operation
AC 2.1	2	6000	
AC 2.2	5	6000	
AC 2.3	10	6000	



Results for analysed Load Cases

Analysis Case	ΔT (K)	Ω (rpm)	Q_{gap} (W)	Q_{goal} ratio
AC 1.1	2	0	44	30 %
AC 1.2	2	1200	31	21 %
AC 1.3	2	3000	43	29 %
AC 1.4	2	6000	58	39 %
AC 2.1	2	6000	58	39 %
AC 2.2	5	6000	103	69 %
AC 2.3	10	6000	150	100 %

Magnetisation mode

Normal Operation

- **The heat transfer in the gap is determined by the speed of the rotor**
- **An increase of the temperature difference in the system results in an increase of the heat transfer**

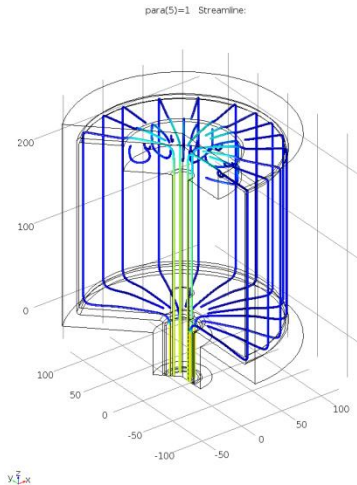
Results: Flow analysis



Magnetisation mode

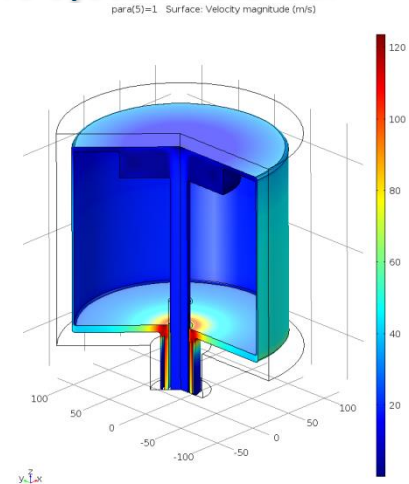
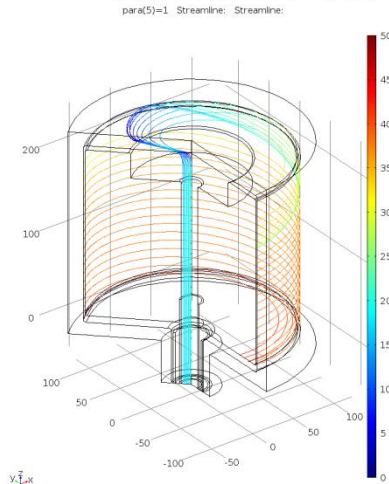
$\Omega = 0$ rpm, $\Delta T = 2$ K

- Pressure flow
- Velocity: axial component
- Pressure drop: 10 mbar



Normal Operation: $\Omega = 6000$ rpm, $\Delta T = 2$ K

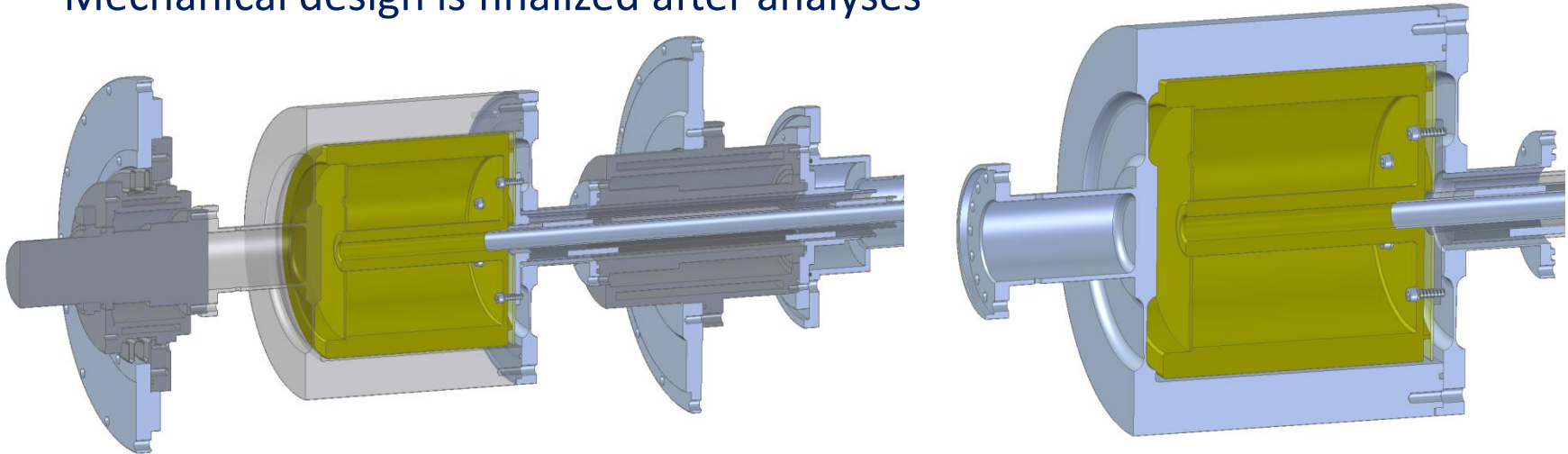
- Pressure and drag flow: axial and phi components
- Swirl at the exit disk
- Back pressure development
 - Pump effect against flow direction
- Pressure increase in the system: 0.5 bar





Conclusions FEM analysis

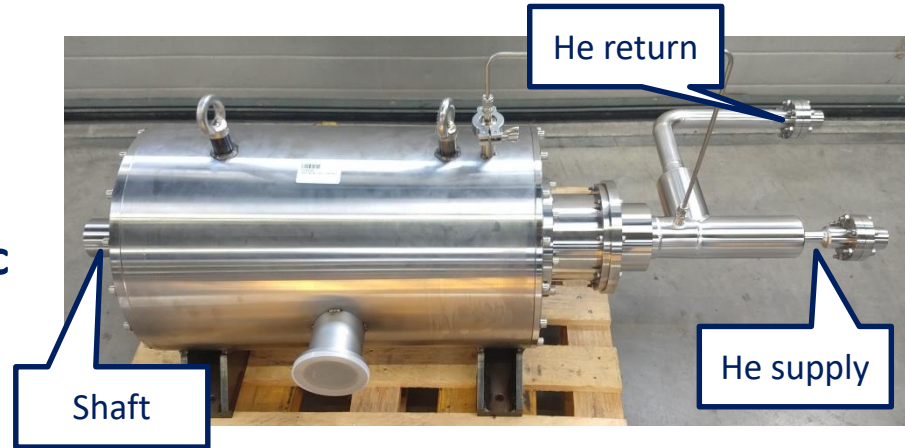
- The Rotor Cooling System
 - Potential to achieve the required cooling power
 - **Experimental validation:** heat transfer and pressure drop
- Mechanical design is finalized after analyses





First hydrodynamic tests

- Rotor speed up to 800 rpm
- **Very good sealing by ferro-fluidic seals** up to 800 rpm:
 10^{-6} mbar/(L.s) level
- More than 1 kW drive power required: significant loss in seals
- No change in pressure drop and flow rate of circulating cooling gas when the rotor speed increases
- **Vortex breaker on exit disk seems effective**





- Continued testing of **Warm Demonstrator**
 - Oswald & Demaco
 - End of the year
- Manufacturing and testing the **Cold Demonstrator**
 - Whole ASuMED consortium
 - First quarter next year

Thank you
for your attention!

